



## Denitrification as an N<sub>2</sub>O sink

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### ABSTRACT

The strong greenhouse gas nitrous oxide (N<sub>2</sub>O) can be emitted from wastewater treatment systems as a byproduct of ammonium oxidation and as the last intermediate in the stepwise reduction of nitrate to N<sub>2</sub> by denitrifying organisms. A potential strategy to reduce N<sub>2</sub>O emissions would be to enhance the activity of N<sub>2</sub>O reductase (NOS) in the denitrifying microbial community. A survey of existing literature on denitrification in wastewater treatment systems showed that the N<sub>2</sub>O reducing capacity ( $V_{maxN2O \rightarrow N2}$ ) exceeded the capacity to produce N<sub>2</sub>O ( $V_{maxNO3 \rightarrow N2O}$ ) by a factor of 2–10. This suggests that denitrification can be an effective sink for N<sub>2</sub>O, potentially scavenging a fraction of the N<sub>2</sub>O produced by ammonium oxidation or abiotic reactions. We conducted a series of incubation experiments with freshly sampled activated sludge from a wastewater treatment system in Oslo and found that the ratio  $\alpha = V_{maxN2O \rightarrow N2} / V_{maxNO3 \rightarrow N2O}$  fluctuated between 2 and 5 in samples taken at intervals over a period of 5 weeks. Adding a cocktail of carbon substrates resulted in increasing rates, but had no significant effect on  $\alpha$ . Based on these results – complemented with qPCR and metaproteomic data – we discuss whether the overcapacity to reduce N<sub>2</sub>O can be ascribed to gene/protein abundance ratios (nosZ/nir), or whether in-cell competition between the reductases for electrons could be of greater importance.

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### 1. Introduction

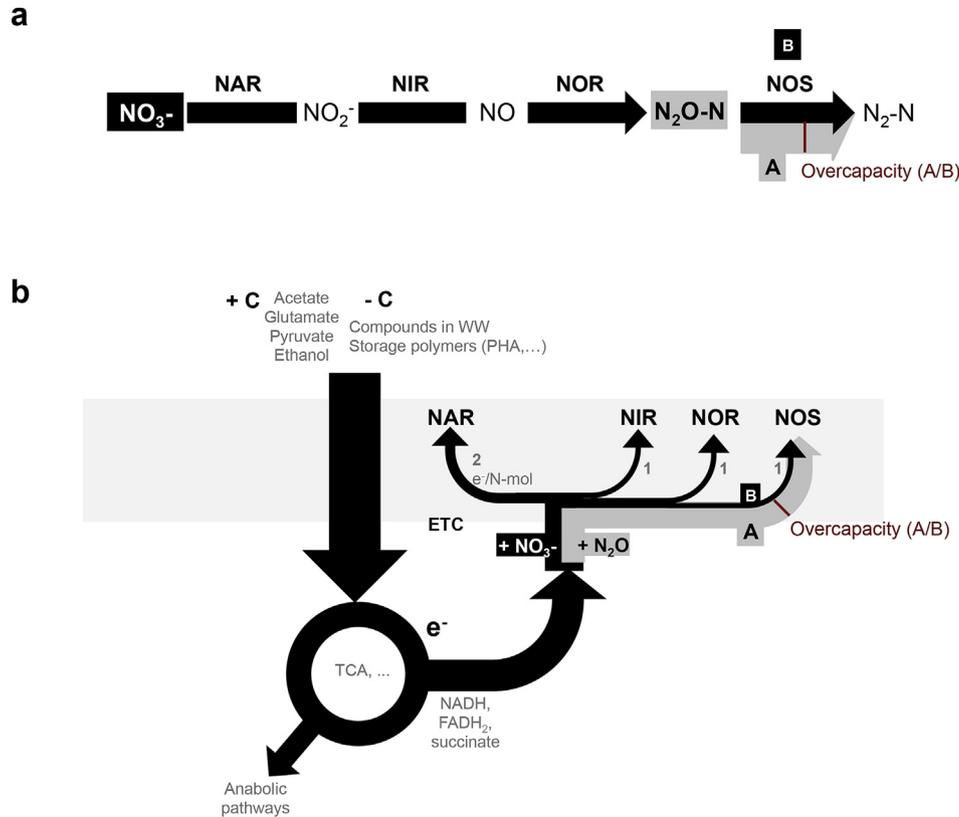
With a global warming potential roughly 300 times greater than CO<sub>2</sub>, N<sub>2</sub>O can be a major contributor to the greenhouse gas footprint of a wastewater treatment plant (WWTP; Daelman et al., 2013). N<sub>2</sub>O accumulates during biological nitrogen removal from wastewater as a byproduct of nitrification by ammonia oxidizing bacteria and/or as a result of incomplete denitrification by heterotrophic denitrifying bacteria in the activated sludge (Kampschreur et al., 2009; Schreiber et al., 2012). The fact that most of the emission of N<sub>2</sub>O occurs in aerated nitrification zones in the full-scale could be taken to suggest that nitrification is the primary source of N<sub>2</sub>O, but this is far from clear since the N<sub>2</sub>O stripped off by aeration could a) originate from non-aerated anoxic zones or b) be produced by denitrification in anoxic microsites within the aerated nitrification zones. Attempts to discriminate N<sub>2</sub>O produced via nitrification or denitrification by isotopomer analyses (Wunderlin et al., 2013) or

by correlating a wide range of process variables to emissions in a long term N<sub>2</sub>O-monitoring campaign in a full-scale WWTP (Daelman et al., 2015) have not been conclusive. Furthermore, N<sub>2</sub>O can be produced via abiotic reactions between intermediates of nitrification and denitrification, e.g. between NO<sub>2</sub><sup>-</sup> and hydroxylamine (Soler-Jofra et al., 2016) or reduced iron species (Kampschreur et al., 2011). The relative contribution of all these different processes to N<sub>2</sub>O accumulation remains unresolved and makes it a challenge to develop greenhouse gas mitigation strategies in full-scale systems.

A number of studies have focused on reducing the production of N<sub>2</sub>O during nitrogen removal (Lu and Chandran, 2010; Perez-Garcia et al., 2017; Ribera-Guardia et al., 2014; Wunderlin et al., 2012) but far fewer have focused on increasing the consumption of N<sub>2</sub>O as an equally valid – and arguably more simple – strategy to reduce emissions. While ammonia oxidizing bacteria (AOB) are invariably net sources of N<sub>2</sub>O, denitrifying organisms are either net sources or net sinks, both producing and consuming this gas (as shown in Fig. 1a). The propensity of a wastewater treatment system, be it of the activated sludge-type or other, to emit N<sub>2</sub>O will be strongly dependent on the intrinsic capacity of its heterotrophic denitrifying

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**Fig. 1.** The denitrification pathway visualized in terms of (a)  $\text{NO}_x$  substrate or (b) electron flow distribution in the ETC. The thickness of black and gray arrows represents the hypothetical proportional flux of N or  $e^-$ -equivalents during incubation with  $\text{NO}_3^-$  (assuming no accumulation of intermediates) or  $\text{N}_2\text{O}$ , respectively and the difference in width in N or  $e^-$  flux through NOS represents a cell or community's overcapacity for  $\text{N}_2\text{O}$  reduction. In (b) we assume that all 4 denitrifying enzymes share a common electron pool. A more complex mixed culture might be partly (or fully) composed of truncated denitrifiers, meaning that the arrows would be segregated in different cells, and different reductases could have access to electron pools of different sizes depending on the cell's metabolic capacity - or preference - to use some electron donor compounds over others.

community to reduce  $\text{N}_2\text{O}$ . A community with low  $\text{N}_2\text{O}$  reductase (NOS) activity relative to the other reductases (i.e. nitrate reductases, NAR, nitrite reductases, NIR, and nitric oxide reductases, NOR) will be a strong  $\text{N}_2\text{O}$ -source, while one with high relative NOS activity will emit less  $\text{N}_2\text{O}$  and may even be able to function as a net sink for  $\text{N}_2\text{O}$  produced during nitrification, as observed in microcosm experiments with Leca-particle biofilms in Mao et al. (2008).

The degree of NOS activity - and the resulting  $\text{N}_2\text{O}$  sink/source strength - of an ecosystem will ultimately depend on a) the genetic potential of the denitrifying community within and/or b) on the overall physiology of said community (including regulation phenomena, enzyme kinetics, electron affinity of the different reductases, etc). Microorganisms can harbor different combinations of denitrification genes in their genome (Graf et al., 2014; Lycus et al., 2017; Roco et al., 2017; Shapleigh, 2013): e.g. denitrifiers lacking the *nosZ* gene encoding NOS are widespread, as are organisms solely equipped with *nosZ* (coined non-denitrifying  $\text{N}_2\text{O}$  reducers in Sanford et al., 2012; Hallin et al., 2018, and referred to as such from here on). Thus, microbial community structure can play a role in the  $\text{N}_2\text{O}$  sink/source potential of a system. But even in denitrifying organisms harboring all the reductases necessary to complete the denitrification pathway (i.e. NAR/NAP, NIR, NOR, and NOS), transcriptional regulation and post transcriptional phenomena may cause an imbalance in the activity of these enzymes, leading to the release of  $\text{N}_2\text{O}$  and/or other intermediate products (i.e.  $\text{NO}_2^-$  and NO; Liu et al., 2013; Lycus et al., 2017). Such imbalances have been associated with e.g. the presence of  $\text{O}_2$ , significant  $\text{NO}_2^-$  accumulation, low C/N ratios, storage polymer metabolism and, not the least, rapid fluctuations in these parameters (Foley

et al., 2010; Kampschreur et al., 2008; Law et al., 2012; Lu and Chandran, 2010; Otte et al., 1996; Wunderlin et al., 2012).

In order to assess the intrinsic  $\text{N}_2\text{O}$  reduction capacity of activated sludge and its potential use in full-scale  $\text{N}_2\text{O}$  emission mitigation strategies, an inventory was made of literature studies reporting maximum conversion rates for  $\text{NO}_3^-$ ,  $\text{NO}_2^-$ , and  $\text{N}_2\text{O}$  in a variety of heterotrophic denitrifying systems. Below we compiled the ratios of maximum rates of  $\text{N}_2\text{O}$  production (from  $\text{NO}_3^-$ ) to  $\text{N}_2\text{O}$ -reduction, which in general were not explicitly reported, as a proxy for the  $\text{N}_2\text{O}$  sink capacity of these systems and calculated the steady state concentrations of  $\text{N}_2\text{O}$  ( $[\text{N}_2\text{O}]_{ss}$ ), an estimation of the  $\text{N}_2\text{O}$ -concentrations at which denitrification changes from being a net source of  $\text{N}_2\text{O}$  ( $[\text{N}_2\text{O}] < [\text{N}_2\text{O}]_{ss}$ ) to become a net sink for  $\text{N}_2\text{O}$  ( $[\text{N}_2\text{O}] > [\text{N}_2\text{O}]_{ss}$ ). Most studies involved lab-scale sequencing batch reactors (SBRs) run for prolonged periods of time, and the resulting microbial population likely had little similarities to that of the activated sludge used as inoculum. An exception is Wicht (1996), who determined  $\text{N}_2\text{O}$  vs.  $\text{NO}_3^-$  consumption rates for activated sludge. However, acetate was used as a sole carbon and energy source, neglecting the contribution of microorganisms unable to use acetate in the  $\text{NO}_3^-$  and  $\text{N}_2\text{O}$  rates reported. In the present study we complement the existing literature by comparing the  $\text{N}_2\text{O}$  and  $\text{NO}_3^-$  conversion rates of fresh activated sludge from a full-scale WWTP, with and without the addition of a mix of organic electron donors, and at 12 °C, a value within the temperature range of the wastewater during most part of the sampling. Furthermore, we address the potential role of (i) the microbial gene and protein abundance in the  $\text{N}_2\text{O}$  sink capacity of the sludge - by quantifying the ratio of *nir* vs. *nosZ* genes and NIR vs. NOS proteins - and (ii) of differences in

electron affinity amongst denitrifying reductases by means of batch tests with the simultaneous addition of  $\text{NO}_3^-$  and  $\text{N}_2\text{O}$ . Based on the results obtained, we discuss the reasons why denitrification is potentially a source of  $\text{N}_2\text{O}$  in full-scale systems, and the possibility of exploiting the  $\text{N}_2\text{O}$  sink potential as a mitigation strategy to reduce emissions of this potent greenhouse gas.

## 2. Materials and methods

### 2.1. $\text{NO}_3^-$ and $\text{N}_2\text{O}$ batch tests with activated sludge

Batch tests were performed in 120 ml serum flasks filled with 50 ml of untreated, undiluted, fresh activated sludge from one of the pre-denitrification tanks of the Bekkelaget WWTP, which is a modified Ludzack-Ettinger (MLE)-type plant in Oslo, Norway (see Figure S1 and for a scheme of the process units, also described in Venkatesh and Elmi, 2013). Samples were taken over a period of 5 weeks in April and May 2015, and later in October 2015 and May 2017. Immediately after sampling, the activated sludge was transported to the lab on ice, dispensed in serum flasks while stirring for sample heterogeneity, and used for batch tests within 4 h after sampling. Preliminary tests showed that conversion rates were not affected by which process unit of the WWTP the activated sludge was obtained from (data not shown).

The flasks, once filled with the 50 ml of activated sludge sample and 3.5 cm long Teflon covered magnets, were sealed with rubber septa and metallic crimps, helium-washed with 6 cycles of vacuum and refilling of the headspace, and placed in the robotized incubation system described in Molstad et al. (2007). After a period of 15 min with stirring at 600 rpm for the temperature of the samples to equilibrate with the surrounding water bath at 12 °C, the flasks were injected with either 1 ml of pure  $\text{N}_2\text{O}$  gas (using a gas tight syringe, aiming for a final headspace concentration of 1%  $\text{N}_2\text{O}$  or 0.9 mM  $\text{N}_2\text{O}-\text{N}$ ) or 1 mM  $\text{NO}_3^-$  (from a 0.5M stock solution of  $\text{NaNO}_3$ ) or both. These batch tests were conducted both with and without the addition of an external electron donor – a mixture of acetate, pyruvate, ethanol and glutamic acid – which was injected into the serum flasks to a final concentration of 0.5 mM for each electron donor, immediately before the injection of  $\text{N}_2\text{O}$  or  $\text{NO}_3^-$ . The transport coefficient for the transfer of gas between the headspace and the liquid was calculated to be  $10^{-3} \text{ L s}^{-1}$  at the stirring speed used - 600 rpm -, meaning that roughly 5–6 min were necessary for the gas-liquid concentrations to reach an equilibrium, as demonstrated in Figure S2. Therefore, to avoid confounding transport and  $\text{N}_2\text{O}$  reduction kinetics a period of 6.3 min was kept between the injection of  $\text{N}_2\text{O}$  and the first sampling of the headspace. Thereafter, the concentration of NO,  $\text{N}_2\text{O}$ ,  $\text{N}_2$ ,  $\text{CO}_2$ , He and  $\text{O}_2$  in the headspace was regularly analyzed by the robotized system and the corresponding concentration of NO,  $\text{N}_2\text{O}$ , and  $\text{N}_2$  in the liquid calculated as described in Molstad et al. (2007). When relevant, 100  $\mu\text{L}$  of slurry sample was collected manually for the immediate determination of  $\text{NO}_3^-$  and  $\text{NO}_2^-$  concentrations (see below). After verifying that results were reproducible (see Figure S3), replicate runs were sacrificed in exchange for a higher time resolution of the conversion rates (the sampling frequency of the robotized incubation system being limited by the length of the GC run and the number of flasks). For our purposes, we only considered the initial consumption rates (i.e. approximately during the first hour of incubation) to avoid the potential effect of changes in enzyme pools or depletion/accumulation of storage polymers (e.g. PHB) on  $\text{N}_2\text{O}$  reduction rates. The buffering capacity of the activated sludge itself was sufficient to maintain the pH in the range of 6.5–7.5 during the batch tests (the initial pH being  $6.5 \pm 0.2$ ; data not shown).

Control experiments with either 15% of acetylene in the

headspace or with autoclaved activated sludge (15 min at 121 °C; both treatments effectively inhibiting NOS activity) were performed.

### 2.2. Analytical procedures

$\text{NO}_3^-$  and  $\text{NO}_2^-$  concentrations were determined by measuring the amount of nitric oxide (NO) produced by the reaction with vanadium (III) chloride in HCl at 95 °C ( $\text{NO}_2^- + \text{NO}_3^-$ ) and the reaction with sodium iodide in acetic acid at room temperature ( $\text{NO}_2^-$  only) using the purger system coupled to the Sievers Nitric oxide analyser NOA280i (Braman and Hendrix, 1989; Cox, 1980).

### 2.3. qPCR and metaproteomics

Activated sludge samples were fixed in 100% ethanol (1 ethanol: 1 sample) and DNA was extracted using FastDNA<sup>®</sup> SPIN Kit for Soil (MP Biomedicals). The primers and PCR conditions used are found in Table S1. Given the potential PCR biases, and the fact that genes are not always expressed, as evidenced by the lacking correlation between gene numbers and related functions in microbial communities (Rocca et al., 2014; Lycus et al., 2017), we also performed an Orbitrap-based mass spectrometry analysis of the proteins. For this, we used a curated database where all the bacterial genera reported to be abundant in activated sludge, anaerobic digesters and influent wastewater (based on MiDAS survey of 24 Danish wastewater treatment plants Mielczarek et al., 2013) were included. The protein extraction procedure aimed at the periplasmic fraction of proteins adapting the protocol for spheroplasts generation (Kučera, 2003). 50 ml of activated sludge was centrifuged at 10 000 g for 20 min and the pellet was used for protein extraction. The pellet was resuspended in 20 ml of 0.1 M Tris-HCl, pH 8.0, 20% sucrose, 1 mM EDTA, 60 mg lysozyme (Fluka) and incubated for 30 min at 37 °C, followed by addition of 25 ml of ice-cold  $\text{H}_2\text{O}$  and gentle mixing by inverting the tube. The sample was then incubated on ice for another 10 min and centrifuged at 10 000 g for 20 min. The supernatant containing water soluble proteins was then concentrated on VivaSpin centrifugal concentrator (Sartorius) with the 30 kDa cutoff. Concentrated prepare was used for proteomic analysis. More details can be found in Supplementary Materials.

### 2.4. Analysis of literature data

We selected studies that reported rates of nitrate reduction in the presence of nitrate excess ( $R_{\text{NO}_3}$ ), and rates of  $\text{N}_2\text{O}$ -reduction under conditions of  $\text{N}_2\text{O}$  excess and absence of other nitrogen oxyanions ( $R_{\text{N}_2\text{O}}$ ), which were taken as estimates of the maximum rates of  $\text{N}_2\text{O}$  production ( $V_{\text{maxNO}_3 \rightarrow \text{N}_2\text{O}}$ ) assuming no significant accumulation of intermediates, and the maximum rates of  $\text{N}_2\text{O}$  reduction ( $V_{\text{maxN}_2\text{O} \rightarrow \text{N}_2}$ ), respectively. We calculated the ratio  $\alpha = V_{\text{maxN}_2\text{O} \rightarrow \text{N}_2} / V_{\text{maxNO}_3 \rightarrow \text{N}_2\text{O}}$  with the data from these studies and we used this data to estimate steady state  $\text{N}_2\text{O}$  concentration during denitrification (at high nitrate concentrations,  $\gg K_s$ , no extra  $\text{N}_2\text{O}$  added). Assuming the gross production of  $\text{N}_2\text{O}$  to be as measured ( $= V_{\text{maxNO}_3 \rightarrow \text{N}_2\text{O}}$ ), and the  $\text{N}_2\text{O}$  reduction rate a simple Michaelis Menten function of the  $\text{N}_2\text{O}$  concentration the following differential equation can be set up:

$$d[\text{N}_2\text{O}]/dt = V_{\text{maxNO}_3 \rightarrow \text{N}_2\text{O}} - V_{\text{maxN}_2\text{O} \rightarrow \text{N}_2} * [\text{N}_2\text{O}] / ([\text{N}_2\text{O}] + k_{\text{mN}_2\text{O}}) \quad (1)$$

Where  $[\text{N}_2\text{O}]$  is the concentration in mol  $\text{L}^{-1}$  of  $\text{N}_2\text{O}$  in the liquid and  $k_{\text{mN}_2\text{O}}$  is the half saturation constant in mol  $\text{L}^{-1}$  for  $\text{N}_2\text{O}$  reductase. Solving for  $[\text{N}_2\text{O}]$  when  $d[\text{N}_2\text{O}]/dt = 0$  the steady state  $\text{N}_2\text{O}$  concentration ( $[\text{N}_2\text{O}]_{\text{ss}}$ ) can be obtained:

$$[N_2O]_{ss} = k_{mN_2O} / (\alpha - 1), \text{ where } \alpha = V_{maxN_2O \rightarrow N_2} / V_{maxNO_3 \rightarrow N_2O} \quad (2)$$

### 3. Results and discussion

#### 3.1. Overcapacity of N<sub>2</sub>O reduction in activated sludge and other denitrifying systems

A number of studies in literature report the maximum rates, as measured in batch tests in the absence of substrate limitation, for the different steps of denitrification in activated sludge (Wicht, 1996) and denitrifying SBRs (Itokawa et al., 2001; Pan et al., 2012, 2013; Ribera-Guardia et al., 2014; Wang et al., 2014). We calculated the ratio  $\alpha = V_{maxN_2O \rightarrow N_2} / V_{maxNO_3 \rightarrow N_2O}$ , which was not explicitly reported in these studies, as an indication of the N<sub>2</sub>O sink (or source) potential of the denitrifying community in these systems. Interestingly the  $\alpha$  values obtained showed that N<sub>2</sub>O reduction rates were consistently higher than the corresponding NO<sub>3</sub><sup>-</sup> reduction rates, by a factor between 2 and 10 (Table 1). We consider  $\alpha$  values > 1 to represent the overcapacity of the N<sub>2</sub>O reduction step relative to the rest of the denitrification pathway (as illustrated in Fig. 1) and a measure of the potential N<sub>2</sub>O sink capacity of the denitrifying community in these systems.

We carried out additional batch experiments to determine the  $V_{maxN_2O \rightarrow N_2}$  and  $V_{maxNO_3 \rightarrow N_2O}$  in freshly sampled activated sludge taken during a 5-week sampling campaign at the Bekkelaget WWTP, and on two subsequent occasions (Fig. 2). The  $\alpha$  values obtained from these tests ranged from 2 to 5, reflecting a persistent N<sub>2</sub>O reduction overcapacity of the activated sludge over time (Fig. 3). The overcapacity was apparent in the batch tests both with and without the addition of a mixture of acetate, pyruvate, glutamic acid, and ethanol carbon substrate (rates increased by a factor of roughly 3–5 in the presence of the carbon substrate – Fig. S4). In the batch tests provided with external N<sub>2</sub>O, the measured rate of N<sub>2</sub>O depletion sometimes exceeded the measured rates of N<sub>2</sub> production by 5–10% (data not shown) and we considered that this could be due to strong sorption of N<sub>2</sub>O to the activated sludge or

conversion via an abiotic pathway other than reduction to N<sub>2</sub>. However tests with acetylene in the headspace or with autoclaved sludge did not provide any evidence for loss of N<sub>2</sub>O and the difference was therefore attributed to error propagation in the calculation of gas-liquid mass transfer of N<sub>2</sub>O from the headspace to the sludge which do not affect the N<sub>2</sub> production rates (Figure S2).

#### 3.2. N<sub>2</sub>O overcapacity and NOS/NIR ratio of the microbial community

The *nosZ* and *nirK* gene abundance in the activated sludge, determined by qPCR, showed that copy numbers of the genes encoding for NOS (*nosZI* + *nosZII*) were higher but in the same order of magnitude as NIR (*nirK* + *nirS*), with a *nosZ*/(*nirS* + *nirK*) abundance ratio of ~2 (Table S2). The abundance of NIR and NOS proteins measured by means of a metaproteomic assay, showed that protein numbers were, on the contrary, greater for NIR than for NOS (1.19\*10<sup>9</sup> NIR vs. 6.4\*10<sup>8</sup> NOS), but nevertheless close to the same order of magnitude. Taken together, the gene and protein abundance data suggests that the efficient N<sub>2</sub>O reduction in activated sludge is likely not a result (i) of a numerical dominance of NOS over NIR or (ii) of a relatively abundant population of non-denitrifying N<sub>2</sub>O reducers in the sludge.

N<sub>2</sub>O overcapacity in the context of electron competition in the electron transport chain.

Electron competition amongst the different denitrifying reductases could create a bias in the N<sub>2</sub>O sink potential reflected in  $\alpha$  (note that the total electron flux for an equivalent amount of N<sub>2</sub>O–N reduction to N<sub>2</sub> is 5 times greater during the batch tests with NO<sub>3</sub><sup>-</sup> than in those provided with only N<sub>2</sub>O). Denitrification is a sequential process in terms of substrates, but a branched process in terms of electron flow within the electron transport chain (ETC; see Fig. 1, a vs. b) and there is evidence that, even under conditions of electron acceptor excess, the electron supply rate to the ETC may not match the combined electron accepting capacity of the denitrifying reductases (Pan et al., 2013). To assess whether a lower affinity of NOS for electrons relative to the other reductases, would

**Table 1**  
Ratio of the maximum N<sub>2</sub>O consumption and production rates (from NO<sub>3</sub><sup>-</sup>) reported in literature and in this study (expressed as  $\alpha$ ) and steady state concentrations of N<sub>2</sub>O ([N<sub>2</sub>O]<sub>ss</sub>) during denitrification in these systems, expressed as a fraction of the culture's K<sub>s</sub> for N<sub>2</sub>O.

Reference	System	C source	Conditions	$\alpha = V_{maxN_2O \rightarrow N_2} / V_{maxNO_3 \rightarrow N_2O}^a$	[N <sub>2</sub> O] <sub>ss</sub> Fraction of K <sub>s</sub> <sup>b</sup>
This study Ribera-Guardia et al. (2014)	Activated sludge Denitrifying SBR <sup>d</sup>	Mix <sup>c</sup> + WW		2–5	0,5–1
		Acetate		3,0	0,5
		Ethanol		3,6	0,38
		Methanol		7,5	0,15
		Mix		3,4	0,41
Pan et al. (2013) Pan et al. (2012)	Denitrifying SBR <sup>d</sup> Denitrifying SBR <sup>d</sup>	Methanol	pH 7	8,4	0,14
		Methanol	pH 6	3,3	0,43
Wang et al. (2014)	Denitrifying SBR <sup>d</sup>	Acetate	pH 7	6,4	0,19
			pH 8	8,6	0,13
			pH 9	10,5	0,11
			4 °C	3,3	0,43
			20 °C	1,9	1,11
Itokawa et al. (2001)	Nitrifying-denitrifying SBR <sup>c</sup>	Acetate	34 °C	1,9	1,11
			COD/N 3.5	2,2	0,83
			COD/N 5.0	3,5	0,4
Wicht (1996)	Activated sludge	Acetate		4,0	0,33
Hassan et al. (2016)	Soil			0,5–5	0,33–∞ <sup>e</sup>
Hassan et al. (2016)	<i>Paracoccus denitrificans</i>	Succinate	NO <sub>2</sub> <sup>-</sup>	2 <sup>f</sup>	0,14

<sup>a</sup> In the literature studies,  $V_{maxNO_3 \rightarrow N_2O}$  was estimated from RNO<sub>3</sub> (see text for explanation).

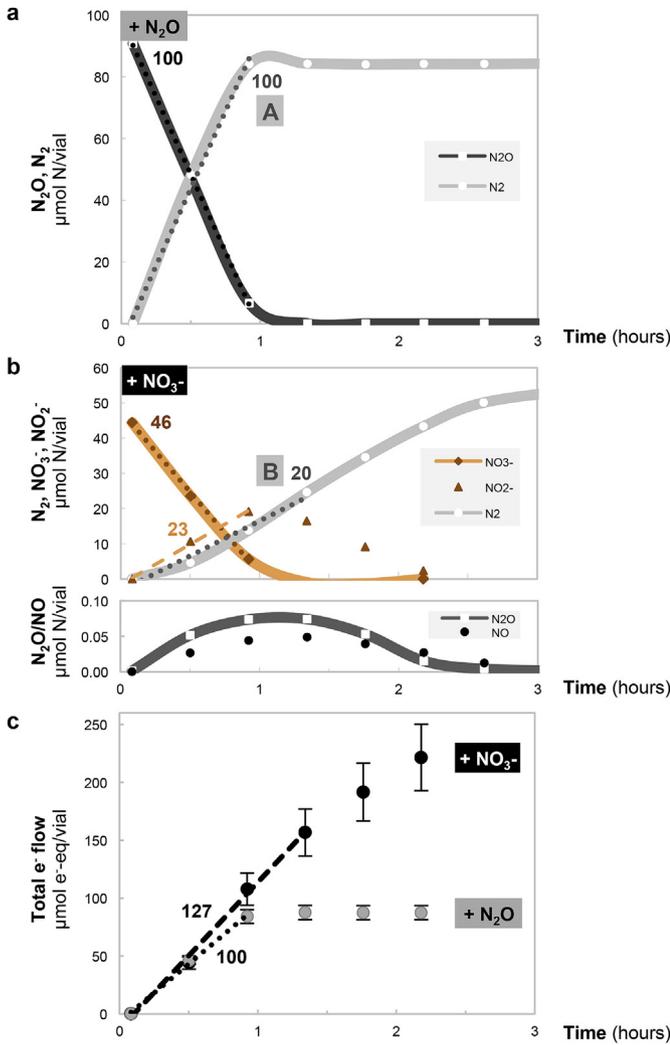
<sup>b</sup> Steady state N<sub>2</sub>O-concentration expressed as fractions of  $k_{mN_2O}$  (see text for explanation).

<sup>c</sup> C source mixture included acetate, ethanol, glutamate and pyruvate.

<sup>d</sup> SBR inoculated with activated sludge.

<sup>e</sup> No steady state concentration is reached if RN<sub>2</sub>O/RNO<sub>3</sub> < 1.

<sup>f</sup> The value is for cultures grown by denitrification through many generations. Much higher  $\alpha$ -values are measured for a period after transition to anoxia because all cells express NOS, while only a fraction express NIR (Hassan et al., 2016).



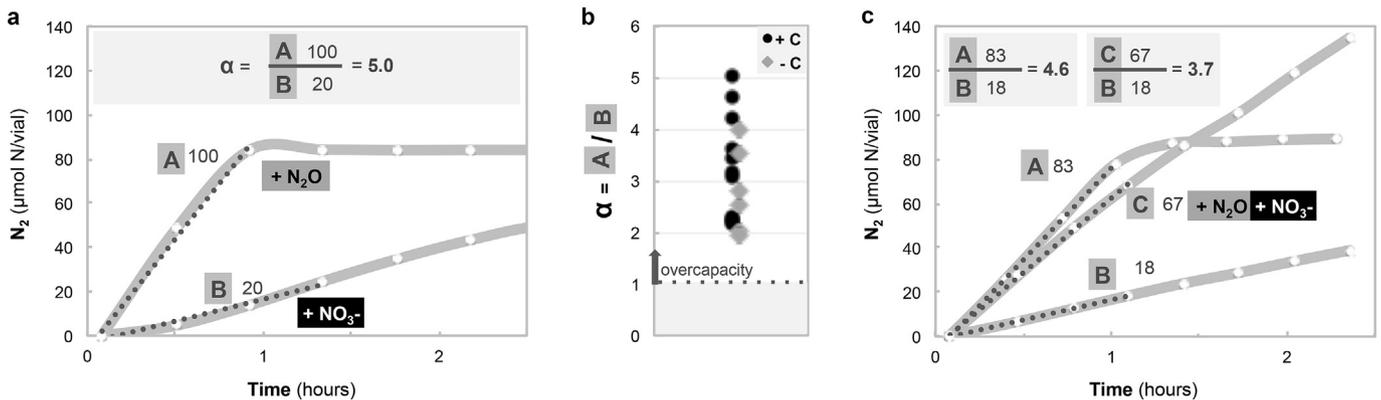
**Fig. 2.** Example of parallel  $N_2O$  (a) and  $NO_3^-$  (b) batch incubation tests with the activated sludge collected on one of the sampling days. The maximum  $N_2O$  reduction and  $N_2O$  production rates of the sludge ( $V_{maxN_2O \rightarrow N_2}$ ; labelled A and  $V_{maxNO_3 \rightarrow N_2O}$ ; labelled B - in  $\mu\text{mol N vial}^{-1} \text{h}^{-1}$ ) were obtained from the linear regression of the data points during the first hour of the experiments (see Fig. 3b). (c) Cumulative electron flux to denitrification in the two treatments.

affect the NOS overcapacity highlighted above (electron competition being absent in our determination of  $V_{maxN_2O \rightarrow N_2}$ ) we performed additional batch tests providing  $N_2O$  and  $NO_3^-$  to the sludge simultaneously. In the presence of both  $N_2O$  and  $NO_3^-$  the total flux going through NOS decreased compared to the  $N_2O$ -only experiments (indicating at least some degree of electron competition) but  $N_2O$  overcapacity persisted, providing evidence that NOS can effectively compete with the other denitrifying reductases (Fig. 3c). Similar conclusions can be reached from the results of batch experiments with denitrifying SBR cultures in Ribera-Guardia et al. (2014) and Pan et al. (2013), though it remains to be seen if the competitiveness of NOS would persist under, for example, more extreme conditions of C limitation, pH, microaerophilic conditions, etc.

### 3.3. Implications for full-scale WWT systems

Given the literature survey and our results, it would seem that (1) a varying degree of  $N_2O$  reduction overcapacity is universal in denitrifying (heterotrophic) communities – true for a broad range of pH and temperature values, COD/N ratios, organic electron donors, and irrespective of whether microbial cultures are exposed to fully anoxic or alternately oxic-anoxic conditions or electron competition phenomena, and (2) that this NOS overcapacity is a physiological characteristic of denitrifying microorganisms rather than a result of the genetic potential of the microbial community. Indeed, NOS overcapacity has also been (non-explicitly) reported for pure cultures of the full-fledged denitrifier *Paracoccus denitrificans*: with conversion rates of  $N_2O \rightarrow N_2$  to 6 times higher than those of  $NO_2^-$  depending on whether the culture had been exposed to oxic conditions shortly before a switch to anoxia or had been growing for a number of generations under anoxic conditions (Bergaust et al., 2012; Hassan et al., 2016).

We are not aware of a conserved regulatory or post-regulatory mechanism hardwiring denitrifying cells to overexpress the  $N_2O$  reduction step relative to the other denitrification steps. The existence of such a mechanism would be a surprising explanation given the diversity of denitrifying regulatory phenotypes found even within a same genus (Liu et al., 2013). Furthermore, given that protein numbers of NOS were lower than NIR, NOS overcapacity is more likely to be a result of enzyme activity or electron affinity than of gene overexpression. Whatever the mechanism behind it, a hardwired NOS overcapacity could be a competitive strategy



**Fig. 3.** Overcapacity on  $N_2O$  reductase activity in the activated sludge samples. (a) Example of how the data from the batch experiments in Fig. 2 was used to calculate  $\alpha$ . For simplicity – we derived  $V_{maxNO_3 \rightarrow N_2O}$  from the production rate of  $N_2$  during the batch tests with  $NO_3^-$ , given that  $N_2O$ -N accounted for less than 1% of  $N_2$ -N produced during the first hour. The  $N_2$  production rate is a proxy for the N or  $e^-$  - equivalent flux through NOS. (b)  $\alpha$  values determined from the  $N_2$  production rates shown in Figure S4 on different sampling days with (+C) and without (–C) the addition of the cocktail of carbon substrates. (c) Example of  $N_2$  production rates during a batch experiment provided with  $N_2O$  (A) or  $NO_3^-$  (B) or both  $N_2O$  and  $NO_3^-$  simultaneously (C).

evolved to maximize the effective electron accepting capacity of denitrifying cells, which could be particularly advantageous in systems like WWTP with frequently fluctuating availability of electron donor and electron acceptor limitations (e.g. we estimated that any given denitrifying species in the Bekkelaget activated sludge would be exposed to oxic/anoxic transitions in the range of 12–104 times per generation - see Figure S1).

Unfortunately, an overcapacity of N<sub>2</sub>O reduction (which reflects maximum conversion rates under substrate excess) is not a guarantee that N<sub>2</sub>O will not accumulate and be emitted to the atmosphere in a wastewater system. The affinity constant ( $K_s$ ) of the culture for the N<sub>2</sub>O determines the steady state N<sub>2</sub>O concentration ( $[N_2O]_{ss}$ ) at which the denitrifying community changes from being a net source of N<sub>2</sub>O to become a net sink, and relatively high steady state N<sub>2</sub>O concentrations during denitrification imply a greater likelihood of N<sub>2</sub>O stripping into the gas phase (the degree of which will depend on the gas-liquid mass transfer of the system). Using the data obtained in literature and in this study, we estimate the steady state N<sub>2</sub>O concentrations to be in the range of 0.1–1.1\* $K_s$  (Table 1), and assuming  $K_s$  values for N<sub>2</sub>O in the range of 0.6–3.4  $\mu$ M (based on  $K_m$  values determined by Hassan et al., 2016 and Pouvreau et al., 2008), this would mean concentrations of 0.07–3.74  $\mu$ M, equivalent to a partial pressure range 2–100\*10<sup>-6</sup> atm at 10 °C (given a solubility of N<sub>2</sub>O of 0.039 mol L<sup>-1</sup>atm<sup>-1</sup>) or a concentration range of 2–100 ppmv of N<sub>2</sub>O in the gas phase (if in equilibrium with the liquid). This relatively low concentration range suggests that denitrification is likely to be a net sink for N<sub>2</sub>O in activated sludge systems, able to consume part of the N<sub>2</sub>O produced by nitrification or abiotic reactions.

The observation that N<sub>2</sub>O reduction overcapacity in denitrifying communities is widespread should be considered in modeling efforts and in the development of N<sub>2</sub>O mitigation strategies during nitrogen removal from wastewater. For example, carousel-type systems, or MLE systems with increased recirculation rates, could be less prone to emissions than e.g. MLE systems with a low recirculation rate since, microbial communities are subjected to more frequent oxic-anoxic shifts. Under such conditions nitrification derived N<sub>2</sub>O would be more rapidly transferred to the anoxic zones and readily consumed by N<sub>2</sub>O reducing microorganisms, instead of being stripped to the atmosphere.

#### 4. Conclusions

- The N<sub>2</sub>O reducing capacity of denitrifying microbial communities generally exceeds their capacity to produce N<sub>2</sub>O by a factor of 2–10, making denitrification a potential N<sub>2</sub>O sink in wastewater treatment systems, scavenging N<sub>2</sub>O derived not only from denitrification but also from ammonium oxidation and abiotic reactions of NO<sub>2</sub><sup>-</sup>.
- Numbers in the same order of magnitude of NIR and NOS, both in terms of genes and proteins, suggest that the overcapacity observed in denitrifying systems is a characteristic of denitrifier physiology, rather than a consequence of the genetic composition of the microbial community.

#### Declaration of interests

X The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

The authors declare the following financial interests/personal relationships which may be considered as potential competing interests:

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#### Appendix A. Supplementary data

Supplementary data to this article can be found online at <https://doi.org/10.1016/j.watres.2018.11.087>.

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